

S45
B6

~~HIGH FREQUENCY PIEZOELECTRIC RESONATOR~~

BACKGROUND OF THE INVENTION

Field of the Invention

5 The present invention relates to a high frequency piezoelectric resonator and, more particularly, to a high frequency piezoelectric resonator that is adapted to suppress the occurrence of spurious.

10 Description of the Related Art

Following making higher the frequency, making higher the speed of data processing, and making larger the capacity, of communication apparatus, there has in recent years been a strong demand for making higher the frequency of a piezoelectric device
15 that is used in each of these apparatus.

Development as to the increase in frequency of an AT cut crystal resonator has been being performed and, during this period of time, the frequency intended to be used therein has hitherto reached several hundreds of MHz. As well known, the
20 waves in the vibration mode of the AT cut crystal resonator are in the thickness shear mode. Therefore, the frequency thereof is in inverse proportion to the thickness of the crystal plate. So, it is necessary to make thin the thickness of the crystal plate in order to make the frequency higher.

25 Figs. 7(a) and 7(b) are views illustrating the construction of a conventional high frequency AT cut crystal resonator, Fig. 7(a) being a plan view and Fig. 7(b) being a

sectional view. Part of a main surface of a crystal plate 21 is recessed using, for example, a photolithography technique and method of etching. The portion of the substrate 21 corresponding to this recess 22 is made to be an ultra-thin vibration portion. This portion of the plate 21 and a thick annular surrounding portion that retains the area around that vibration portion are formed integrally with each other. On one main surface (flat surface) of the crystal plate 21 there is disposed an electrode 23. From the electrode 23 there is extended toward the edge of the plate 21 a lead electrode 25. Further, on the other surface of the substrate 21, i.e., on the surface having therein the recess 22, there is formed an entire electrode 24.

It is to be noted that the energy trapping of the AT cut high frequency crystal resonator having a structure illustrated in Fig. 7, as well known, depends only upon the mass loading of the electrode 23 and not upon the mass loading of the entire electrode 24 on the other surface.

Fig. 8 is a view illustrating a measured example of the frequency spectrum of the AT cut high frequency crystal resonator having the structure illustrated in Fig. 7. The resonance frequency is set to be 156.6 MHz (the thickness of the crystal plate 21 is set to be approximately 10 μ m); the dimension in the X-axial direction of the electrode 23 is set to be 0.55 mm; the dimension in the Z'-axial direction is set to be 0.435 mm; and as the electrode 23 there was adhered a thin film of gold having a thickness of 600 Å on a backing layer

of nickel having a thickness of 50 Å. It is to be noted that the material of the film constituting the entire electrode 24 was also formed substantially in the same way.

As obvious from the frequency spectrum of Fig. 8, from the fundamental mode up to a large number of inharmonic modes fall within the range of the energy trapping mode. These modes, as seen, are sharply excited as spurious. Using this crystal resonator as one component of the oscillator, there is the possibility that the phenomenon of the frequency jump will occur.

As a method of analyzing a spurious mode in the thickness shear resonator such as that illustrated in Fig. 8, there is well known an energy trapping theory, which will briefly be explained below.

Fig. 9 is a sectional view illustrating the section of an ordinary AT cut crystal resonator. The diameter of a circular crystal plate 31 having a thickness of H is set to be 2b; the diameter of an electrode 32 that has been adhered thereto is set to be a; and the cutoff frequencies of the electrode 32 portion and the plate 31 portion are set to be f_1 and f_2 , respectively. Generally, the plate-back Δ , the energy trapping coefficient ζ and the normalized frequency ψ are expressed as follows.

$$\Delta = \frac{(f_2 - f_1)}{f_1} \quad \dots\dots\dots (1)$$

$$\zeta = \frac{na}{H} \sqrt{\Delta} \quad \dots\dots\dots (2)$$

$$\phi = \frac{(f-f_1)}{(f_2-f_1)} \dots\dots\dots (3)$$

In the equation No. 2, n represents the order of the overtone mode. When the mode is the fundamental mode, n=1. Fig. 10 illustrates a frequency spectrum of the crystal resonator having the structure of Fig. 9, as determined by calculation, with the energy trapping coefficient ζ being plotted along the abscissa and the normalized frequency ψ being plotted along the ordinate. Generally, in order to design an resonator wherein spurious less occur, using the energy trapping coefficient $\zeta=0.707$ that is immediately before the symmetrical 1st mode S_1 starts to be trapped is admitted as being preferable.

Here, Fig. 10 illustrates the results that have been obtained by the calculation that has been performed on the premise that the substrate be an isotropic elastic body. However, if applying this method of determining the frequency spectrum to an anisotropic piezoelectric plate such as a crystal, it is well known that it is sufficient to multiply each length by an anisotropic constant to thereby correct this length. For instance, with respect to the thickness twist mode and the thickness shear mode of the crystal resonator, their respective optimum energy trapping coefficients ζ are said to be 2.4 and 2.8.

Determining the energy trapping coefficient ζ of the high frequency crystal resonator illustrated in Fig. 8 according to the equation (2) as a trial, the $\zeta=5.7$. It is seen that this value is the one that is much greater than the optimum value.

Therefore, as stated above, a high order of vibration mode also becomes an energy-confining mode, whereby a large number of spurious are sharply excited.

On the other hand, in order to improve the spurious characteristic of the AT cut crystal resonator, a piezoelectric resonator that can somewhat arbitrarily control the frequency of the generated spurious regardless of the length, film thickness, etc. of the electrode has been proposed in Japanese Patent Application Laid-Open Nos. Hei-9-27729 and Hei-9-93076.

Fig. 11(a) is a plan view illustrating a crystal resonator that is as proposed above and Fig. 11(b) is a sectional view thereof. On both surfaces of the central parts of a crystal plate 41 there are disposed main electrodes 42a and 42b. Simultaneously, second electrodes 44a and 44b are disposed so as to surround the peripheral edges of those electrodes 42a and 42b and with a gap between the both. The respective cutoff frequencies of the main electrodes 42a, 42b, gap portion, and second electrodes 44a, 44b are set to be f_1 , f_2 , and f_3 , as illustrated in Fig. 11(b). Here, the thickness of the electrode films are set so that the relationship among the cutoff frequencies of $f_1 < f_3 < f_2$ holds true among the cutoff frequencies.

Also, the second amount Δ_2 of decrease in frequency and the depth v of the gap (hereinafter referred to as "a groove depth") are respectively defined as follows.

$$\Delta_2 = \frac{(f_3 - f_1)}{f_1} \quad \dots\dots\dots (4)$$

$$\nu = \frac{(f_2 - f_3)}{(f_3 - f_1)} \dots\dots\dots (5)$$

According to the above official gazettes, whatever value the mass loading (the film thickness) of the main electrode 42a, 42b is set to be at, only if appropriately setting the mass loading (the film thickness) of the second electrode 44a, 44b correspondingly, it becomes possible to decrease the amount $\Delta 2$ of decrease in frequency, which participates in the energy trapping coefficient ζ , down to a desired value. The above official gazettes describe that therefore it becomes possible to easily control the energy trapping coefficient ζ and hence to manufacture a crystal resonator the spurious of that are less. Further, the above official gazettes describe that, by aptly setting the groove depth ν and the ratios q/a and b/a of the distance q and b of the main electrode 42a, 42b with respect to the both edges of the second electrode 44a, 44b, it is possible to somewhat arbitrarily control the value of the energy trapping coefficient ζ permitting the generation of a symmetric high-order mode and anti-symmetric mode. Therefore, if adopting this proposal, it results that only desired main vibration waves can be excited with a high level of power without making an inharmonic mode trapped mode.

However, applying the above proposal to a high frequency 150-MHz band crystal resonator and determining the plate-back $\Delta 2$ using the electrode configuration of Fig. 8 with the energy trapping coefficient ζ being set to be 0.521, this plate-back $\Delta 2$ becomes $\Delta 2 = 0.00144$. If using a thin film of gold for both

the main electrode and the second electrode, the difference in film thickness between the main electrode and the second electrode becomes 21.8 \AA . To realize this difference in film thickness, a precision of 10% or so becomes necessary with
5 respect to the value of the difference. This value goes beyond a limit of control that is possible with an ordinary evaporating or sputter apparatus. Also, even when having used the value, which is immediately before the S_1 mode is trapped, as the energy trapping coefficient ζ , recognizing the generation of the
10 oblique-symmetrical A_0 mode, the difference in film thickness between the main electrode and the second electrode is as very small as 40 \AA . Controlling such a small film thickness difference with a precision of 10% or so is virtually impossible. Even if a film-forming apparatus enabling such control to be
15 made has been developed, there was the problem that such an apparatus became very expensive.

Also, in case that forming a AT cut high frequency crystal resonator such as that illustrated in Fig. 7 using method of etching, the crystal plate prior to etching is etched until its
20 thickness becomes 10 \mu m while maintaining the surface configuration of the substrate, for example, 80 \mu m thick as it is. Therefore, the unevenness in the flatness and the parallelism, which did not become very problematic with the substrate 80 \mu m thick, becomes relatively very greatly
25 problematic when the same is viewed from the etched plate that has become 10 \mu m thick. Resultantly, anti-symmetrical modes A_0 and A_1 of vibration, which in an ordinary crystal resonator

didn't become problematic due to cancellation of the electric charges, appear as vigorous spurious in the thin portion which vibrates. For this reason, the following problem arose.

Namely, as the energy trapping coefficient ζ that is optimum to suppressing the occurrence of spurious, the value that is immediately before the symmetrical 1st mode S_1 starts to be trapped is not adequate. In other words, a sufficiently small value of energy trapping coefficient ζ must be used so that the anti-symmetric mode A_0 does not become trapped.

10

SUMMARY OF THE INVENTION

The present invention has been made in order to solve the above-described problems and has an object to provide an AT cut high frequency crystal resonator wherein the occurrence of spurious is less.

15

To attain the above object, according to the first aspect of the invention, there is provided a high frequency piezoelectric resonator, the piezoelectric resonator including a piezoelectric plate having disposed on its main surfaces, respectively, mutually opposing main electrodes for the excitation, a pair of second electrodes being each disposed surrounding the peripheral edge of its corresponding main electrode with a gap in between, wherein the material of the main electrode and the material of the second electrode are different from each other.

20

25

According to the second aspect of the invention, there is provided a high frequency piezoelectric resonator according

to the first aspect, wherein the density of the material of the second electrode is made lower than that of the main electrode.

According to the third aspect of the invention, there is provided a high frequency piezoelectric resonator according to
5 the first or second aspect, wherein the piezoelectric plate is made a piezoelectric plate having formed therein a recess.

According to the fourth aspect of the invention, there is provided a high frequency piezoelectric resonator according to the first to third aspects, wherein the configuration of the
10 main electrode is made elliptic.

According to the fifth aspect of the invention, there is provided a high frequency piezoelectric resonator including a piezoelectric plate, one main surface of the piezoelectric plate being recessed to thereby form a thin portion therein,
15 the main surface opposing the recess corresponding to the thin portion having formed thereon at its central portion a convex portion, the convex portion having formed thereon a main electrode for the excitation, a lead electrode being extended from the main electrode toward an edge of the plate, a second
20 electrode being so provided as to surround the main electrode and the lead electrode with a gap in between, the piezoelectric plate having applied on a recess side thereof an entire electrode.

According to the sixth aspect of the invention, there is
25 provided a high frequency piezoelectric resonator according to the fifth aspect, wherein the convex portion is made elliptic.

According to the seventh aspect of the invention, there

is provided a high frequency piezoelectric resonator according to the first to sixth aspects, wherein the second electrode is divided into a plurality of portions; and adjustment of frequency is performed of these electrode portions.

5 BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1(a) is a plan view illustrating the construction of an AT cut high frequency crystal resonator according to the invention, and Fig. 1(b) is a sectional view thereof;

Fig. 2 is a view illustrating a frequency spectrum of the
10 crystal resonator having a structure of Figs. 1(a) and 1(b), the frequency spectrum being the one that has been obtained by calculation;

Fig. 3 is a view illustrating a frequency spectrum of the
15 crystal resonator having a structure of Figs. 1(a) and 1(b), the crystal resonator being the one that has been manufactured and the frequency spectrum of that has been measured;

Fig. 4 is a plan view illustrating the construction of a second embodiment of the invention;

Fig. 5 is a plan view illustrating a main part of the
20 construction of a third embodiment of the invention;

Fig. 6(a) is a plan view illustrating the construction of a fourth embodiment of the invention, and Fig. 6(b) is a sectional view thereof;

Figs. 7(a) and 7(b) are views illustrating the
25 construction of a conventional AT cut high frequency crystal resonator, Fig. 7(a) being a plan view thereof and Fig. 7(b) being a sectional view thereof.

Fig. 8 is a view illustrating a frequency spectrum of the conventional AT cut high frequency crystal resonator;

Fig. 9 is a sectional view illustrating a crystal resonator for explaining an energy-confining theory;

5 Fig. 10 is a view illustrating a frequency spectrum of a conventional crystal resonator, the frequency spectrum being the one that has been obtained by calculation; and

Figs. 11(a) and 11(b) are views illustrating the construction of a conventional spurious suppression type piezoelectric resonator, Fig. 11(a) being a plan view thereof and Fig. 11(b) being a sectional view thereof.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

15 The present invention will now be explained in detail on the basis of the embodiments illustrated in the drawings.

Sub BV
20 Figs. 1(a) and 1(b) are views illustrating the construction of an AT cut high frequency crystal resonator according to the invention, and Fig. 1(a) being a plan view thereof and Fig. 1(b) being a sectional view taken along a line Q-Q. On a flat-surface side of a crystal plate 1 the other surface of that has formed therein a recess, there is disposed a main electrode (an excitation electrode) 2. From the electrode 2 there is extended toward an edge of the plate 1 a lead electrode 3. Further, a second electrode 5 is so provided
25 as to surround the peripheral edge of the main electrode 2 with a gap 4 in between. The size of the electrode 5 is made substantially the same as that of the recess 6 formed in the

substrate 1. And, on a recess side there is formed an entire electrode (an excitation electrode) 7.

The respective dimensions of the main electrode 2, gap 4, and second electrode 5 are set as illustrated in Fig. 1(b).
5 Namely, the thickness of the crystal plate 1 is set to be H, and the respective configurations of the main electrode 2, gap 4 and second electrode 5 are each made symmetrical with respect to a Z'-axial direction. Further, the length from a center of the main electrode 2 to an edge of it is set to be a; and the
10 dimensions from the center of the main electrode 2 to an inner side edge and an outer side edge of the second electrode 5 are respectively set to be q and b.

The characterizing feature of the present invention resides in that the material quality of the main electrode
15 (excitation electrode) 2 and that of the second electrode 5 are differentiated from each other. More specifically, the characterizing feature is that the second electrode 5 has been formed using a material constructed of a film, the density of that is lower than that of the film that the main electrode 2
20 is constructed of. For example, taking the aging of the crystal resonator into consideration, a thin film of gold is used as the material of the main electrode 2 and a thin film of silver is used as the material of the second electrode 5 whose effect upon the aging characteristic is small. Because the density
25 of gold and that of silver are respectively 19.32g / cc and 10.50g / cc, constructing like that, the film thickness of the second electrode 5 becomes approximately twice as large as the

thickness of the main electrode 2. Therefore, compared to a case where having used a thin film of gold as each of the both electrodes, it becomes much easier to control the thickness of each film that takes part in energy trapping.

5 To restrict the object waves of the energy-trapped mode to only the main vibration alone, it is necessary to make the film thickness of the second electrode 5 greater than that of the main electrode 2. But it is necessary to set the cutoff frequencies of the both electrodes so that the cutoff frequency
10 f_3 of the second electrode 5 may be higher than the cutoff frequency f_1 of the main electrode 2. Assuming that f_2 represents the cutoff frequency of the gap portion 4, it is necessary that the relationship among the respective cutoff frequencies be $f_1 < f_3 < f_2$.

15 Here, it is confirmed by simulation to what extent the control of the film thickness becomes easy compared to that of the conventional piezoelectric resonator.

Sub B2
20 Setting the center of the main electrode 2 to be the origin (0) and the dimensions of the respective electrode portions to be as stated previously as illustrated in Fig. 1(b) and assuming that the crystal plate 1 be an isotropic elastic body, one dimensional analyses of the thickness shear mode were performed. In the Japanese Patent Application Laid-Open No. Hei-9-27729 that is previously cited, analysis is made using the frequency
25 equation that has been established under the assumption that the edge of the plate 1 be a free edge. However, in the case of a resonator wherein the periphery of the vibration portion

is retained by the annular surrounding portion as in the invention, the frequency equation should be established under the assumption that the edge of the vibration portion be a fixed edge. Accordingly, the frequency equation is as follows.

$$\frac{k_2}{k_1} \cot k_1 a = \frac{\tanh k_2 (q-a) + \frac{k_2}{k_3} \tanh k_3 (b-q)}{1 + \tanh k_2 (q-a) \cdot \frac{k_2}{k_3} \tanh k_3 (b-q)} \dots\dots\dots (6)$$

5

In this frequency equation, through the assumption that the edge of the plate be a fixed edge, the phenomenon that the waves are reflected by the edge surface and the phase thereof is inverted there is taken into consideration. Here, the wave numbers k_1 , k_2 , and k_3 are respectively the propagation constants (wave numbers) of the main electrode 2 portion, gap 4 portion, and second electrode 5 portion.

10

Fig. 2 illustrates the frequency spectra of the main vibration S_0 , anti-symmetric 0th mode A_0 , and symmetric 1st mode S_1 under the assumption that $b/a=1.7$ and $q/a=1.18$ respectively representing the ratios between the length values and $v=29.4$ representing the groove depth be used as the parameters and that ζ representing the energy trapping coefficient be plotted along the abscissa and ψ representing the normalized frequency be plotted along the ordinate. Here, the normalized frequency ψ' is expressed as the following equation.

15

20

$$\phi' = \frac{(f - f_1)}{(f_3 - f_1)} \dots\dots\dots (7)$$

It is to be noted that, as stated previously, the energy trapping coefficient ζ of the abscissa is given as a value that has been obtained using an isotropic plate, and that, in case
 5 that having used a substrate having anisotropy such as that made of crystal, this value has only to be corrected by multiplying the energy trapping coefficient ζ by an anisotropy constant.

Another characterizing feature of the present invention resides in that there has been changed the value of the energy
 10 trapping coefficient ζ that has hitherto been generally accepted in order to suppress the anti-symmetric mode. When the resonance frequency becomes as high as 150 MHz, unlike the contents that are stated in the Japanese Patent Application Laid-Open Nos. Hei-9-27729 and Hei-9-93076, the unevenness in
 15 the flatness and the parallelism of the plate occurs and the lead electrode 3 comes to participate in the generation of the anti-symmetric mode. Resultantly, the anti-symmetric mode becomes also excited. The reason for this is as follows. When the physical symmetry collapses due to the unevenness in the
 20 flatness and the parallelism of the plate or to the lead electrode, the anti-symmetric mode does not become a complete anti-symmetric mode either. Resultantly, the produced electric charges are not completely mutually cancelled by the electrode, with the result that an anti-symmetrical mode
 25 becomes excited.

Therefore, as the value of the energy trapping coefficient ζ , it becomes necessary to use not a value that is immediately before the S_1 mode starts to be trapped and that is conventionally generally accepted but a value that is smaller than that value. Namely, using this smaller value, it becomes necessary to suppress the production of the anti-symmetric A_0 mode. Desirably, as the value of the energy trapping coefficient ζ , a value that is immediately before the waves in the anti-symmetric A_0 mode starts to be trapped is used. Namely, if under the conditions illustrated in Fig. 2 wherein $b/a=1.7$, $q/a=1.18$, and $v=29.4$, the value of the energy trapping coefficient $\zeta=0.67$ or so is optimum. The value of the optimum energy trapping coefficient ζ of the high frequency piezoelectric resonator according to the invention cannot primarily be determined, unless the relevant conditions such as b/a , q/a , or v are determined, unlike the case where the resonator uses a single electrode.

Fig. 3 is a view illustrating a frequency spectrum of the AT cut high frequency crystal resonator according to the invention. The resonance frequency is set to be 156.6 MHz (the thickness of the crystal plate 1 is set to be approximately 10 μm) while the dimension in the X-axial direction and the dimension in the Z'-axial direction of the electrode 2 are set to be 0.55 mm and 0.435 mm, respectively. As the electrode 2, there is adhered a backing layer made of nickel 50 \AA thick and there is adhered thereon a thin film of gold 600 \AA thick. As the second electrode 5, there is adhered a backing layer of

nickel 50 Å thick and there is adhered thereon a film of silver 1100 Å. The dimensions of the respective portions are set such that $b/a=1.7$; and $q/a=1.18$. At this time, the energy-trapping coefficient ζ is 0.521, and it is seen from Fig. 2 that the anti-symmetric 0th mode A_0 is not confined. It is to be noted that the films constituting the entire electrode 7 have been formed substantially in the same way as in the case of the films constituting the main electrode 2.

Comparing to Fig. 8, it is seen that although the constant of the main electrode 2 is the same, the production of the spurious is excellently suppressed. At this time, the equivalent resistance R_1 of the main vibration is approximately 15Ω. So, no deterioration of the equivalent resistance of the main vibration due to the suppression of spurious was confirmed.

Also, the thickness of the film of gold of the main electrode 2 is 600 Å and the thickness of the film of silver of the second electrode 5 is 1100 Å. Namely, unlike the above-described official gazettes, in the present invention, both the main electrode and the second electrode have a film thickness that is sufficiently controllable and can therefore be easily manufactured with a conventional evaporating or sputter apparatus.

Fig. 4 is a plan view illustrating the construction of a second embodiment of the invention. In this second embodiment, the second electrode 5 of Fig. 1 is divided to thereby provide divisional electrodes $5'$, $5'$, ..., and lead electrodes T1, T2, T3, and T4 are provided with respect thereto. In case that there

are slight irregularities or unevenness in the flatness and the parallelism of the crystal plate 1, or in case that there is non-uniformity in the films of the electrodes, the production of spurious due to the anti-symmetric mode can be suppressed
5 by adjusting the frequencies of the second electrode 5', 5', ... For instance, in case that spurious has occurred in a high frequency resonator that has been manufactured, the following countermeasures can be taken. Using the terminals T1, T2, T3, and T4 illustrated in Fig. 4, there is measured the frequency
10 of such resonator. And only if finely adjusting the high-value portions of this frequency by methods of evaporating, etc. it would be sufficient.

Fig. 5 is a plan view illustrating the main electrode and
second electrode constituting a main part of the piezoelectric
15 resonator according to a third embodiment of the present invention. The difference of Fig. 5 from Fig. 1 is that an elliptic main electrode (an excitation electrode) 2a is disposed as the main electrode (excitation electrode) 2 illustrated in Fig. 1(a). This difference further resides in
20 that an elliptic groove hole is formed in the central part of the plate so as to surround the peripheral edge of the main electrode 2a with a gap. That difference further resides in that a second electrode 5a substantially corresponding to the recess 6 of the piezoelectric plate 1 is disposed around the
25 main electrode 2a with the elliptic groove hole in between. That an entire electrode is disposed over the recess of the piezoelectric plate is the same as in Fig. 1.

Sub
B47

The reason for having made the main electrode 2a elliptic is as follows. Determining the two-dimensional vibration displacement distribution of the main vibration, as an attempt, by applying a finite element method, it is seen that the
5 displacement distribution of the main vibration is elliptical due to the anisotropy of the crystallographic axis of the piezoelectric plate. Therefore, manufacturing a high frequency resonator wherein the main electrode and second electrode are each formed elliptic in conformity with the
10 displacement distribution of the main vibration, the production of spurious is suppressed. Resultantly, a resonator whose capacitance ratio is minimal is obtained.

Also, Fig. 6(a) is a plan view illustrating the construction of a fourth embodiment of the present invention
15 and Fig. 6(b) is a sectional view taken along a line Q-Q. Using methods of etching, etc., on a substantially central part of one main surface of the crystal plate 1 there is formed a convex portion T and, on the other main surface thereof, there is formed a recess 6. Thereafter, on the convex portion T, there is
20 disposed a main electrode (an excitation electrode) 2b, and, from the electrode 2b, there is extended toward the edge of the crystal plate 1 a lead electrode 3b. Thereafter, a second electrode 5b is so provided as to surround the peripheral edges of the main electrode 2b and the lead electrode 3b in such a
25 way as to provide a gap between the both. Further, an entire electrode (an excitation electrode) 7 is formed on a recess side of the crystal plate 1, to thereby construct a high frequency

crystal resonator.

Sub
BS
5 The characterizing feature of the fourth embodiment is
as follows. After forming the convex portion T on the
piezoelectric plate 1 beforehand, the main electrode 2b is
10 formed on the convex portion T. Therefore, even when making
the main electrode 2b, lead electrode 3b, and second electrode
5b the same in material quality and in film thickness, the
respective cutoff frequencies thereof have the relationship of
 $f_1 < f_3 < f_2$. Resultantly, it has become possible to
15 satisfactorily achieve the relevant edge by performing the
evaporating or sputtering and photolithography, respectively,
only once.

Also, the cutoff frequency f_1 of the main electrode 2b
region and the cutoff frequency f_3 of the lead electrode 3b
15 region are made to be in a relationship of $f_1 < f_3$. Resultantly,
it has become possible to decrease the leaking vibration energy
of the main vibration by propagating the lead electrode region
3b. Resultantly, it is advantageously possible to not only
suppress the production of spurious but also make greater the
20 Q value of the main vibration at the same time.

In Fig. 6(a), illustration has been made of the
rectangular main electrode 2b. However, the present
inventor's simulation and experiment performed using a finite
element method have confirmed that the capacitance ratio or
25 spurious is able to be improved if forming an elliptic electrode
such as that of Fig. 5 as the main electrode.

In the foregoing description, an explanation has been

given of an example wherein the invention has been applied to the high frequency fundamental crystal resonator in 150 MHz band. However, the invention is not limited to this resonator only but can be also applied to a crystal resonator of every frequency
5 and of overtone in VHF band and UHF band.

Also, in the foregoing description, an explanation has been given of a case where a recess is formed in one surface of the crystal plate. However, the invention can needlessly to say be also applied to a case where a recess portion is formed
10 in each surface of the crystal plate. Also, the configuration of the main electrode and second electrode is not limited to a rectangular configuration alone but may be a circular configuration. Further, a case where an entire electrode has been applied to the recess side has been explained. However,
15 onto each surface, there may be applied a partial electrode. Although a case where gold and silver are used as the material of the electrodes has been explained, the material of the electrodes may be aluminum, titanium, copper, etc. or an alloy of these elements. Also, the method of forming a film or films
20 for the electrodes by the use of such material may be any given type such as evaporating, or sputtering.

Although in the foregoing description a high frequency resonator has been explained, it is obvious that when applying the invention to a high frequency multiple-pole monolithic
25 filter there is the effect of spurious being suppressed.

Since the present invention has been constructed as described above, manufacturing an AT cut high frequency crystal

resonator with spurious being kept suppressed has become possible. If using the crystal resonator of the invention in a voltage controlled crystal resonator, etc., the excellent effect that a high-stability, high frequency, and broadband
5 VCXO apparatus can be manufactured is brought about.